# ENGINEERED PUMPABLE pHOAM $^{TM}$ : A NEW INNOVATIVE METHOD FOR MITIGATING ARD $^1$

James Gusek<sup>2</sup>, Brian Masloff, and John Fodor

**Abstract.** If one can embrace the medical analogue, much of the mining industry currently suffers from a massive bacterial infectio n. When pyrite-bearing or sulfide-bearing rock formations, tailings, or mine wastes are infected by Acidithiobacillus ferro-oxidans, the likelihood of forming acid rock drainage (ARD) is almost guaranteed. The "pharmacy" of anti biotics available is extensive, ranging from solid alkaline amendments 1 ike limestone to liquid "medicines" such as sodium lauryl sulfate, sodium t hiocyanate, waste milk, and bipolar lipids. Unfortunately, the "geo-medical" t eams of geochemists, microbiologists, engineers, and mine managers lack the tools to surgically apply with a minimum of waste. these active ingredients where they are needed most Distribution of fine grained limestone on the surfa ce of an acidic mine waste dump is analogous to applying a bandage soaked in a ntacid to treat an upset stomach. The implementation of up-to-date best mana gement practices has not healed the patient; an equivalent combination of hy podermic needle, cyber knife, and arthroscopic probe is clearly needed.

Using an engineered, flow-able or pumpable foam or pHoam<sup>TM</sup> as the medicinally analogous "dextrose delivery solution" for solid an d/or liquid "geo-antibiotics", the authors have combined off-the-shelf technologie s that have been previously applied in solving geotechnical problems in the min ing industry. A patent for the innovative process is pending. This paper discusse s method concepts and the advantages it could provide over conventional BMPs.

Preliminary laboratory test results suggest that the delivery of solid and liquid materials into porous, unsaturated rock can provide a variety of ARD-suppressing coatings.

The timing of ARD-suppressing materials' applicat ion to ARD-prone wastes in the mining and processing cycle may govern whether these materials behave as a post-infection medicine or as a vaccine that preven ts infection altogether. Field demonstration sites are being sought.

Additional Key Words: acid rock drainage suppression, heavy metals, mi ning influenced water

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#### **Introduction**

Water pollution associated with mining activity has been a problem for societies probably since pre-historic times although it may have not been recognized at the time. The pioneering hard rock miners in the Colorado Rockies recognized the impacts from poor water quality; the water entering some of their underground workings we as so metal-laden and acidic that they could not use it to feed their boilers. In some mines, acid water dissolved iron rails, plating out dissolved copper in the process. In the 16th century, the author G. Agricola in his book De Re Metallica, noted that water contaminated by mining activities "poisons the brooks and streams, and either destroys the fish or drives them away".

Modern mining activities, both coal and hard rock, can generate much the same problem, but with the large volumes of ore and waste rock being excavated and moved, the impacts to the environment are magnified a billion-fold. It is commonly referred to as acid rock drainage or ARD. The sources of water pollution/ARD included raining adits and tunnels, leachate from waste rock and tailings/coal refuse facilities, and water accumulating in or discharging from abandoned pits. Even the construction of highways in geological terrain containing pollution generating rocks has been identified as a problem. The Tennessee Department of Transportation commissioned a guideline document which focused on pollution prevention and ARD mitigation best management practices (Gusek et al., 2008).

## ARD Formation

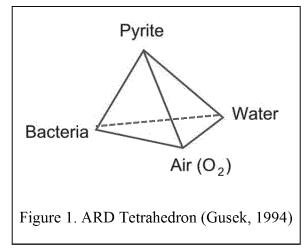
The formation of ARD is a natural process. In the presence of air, water, and bacteria, sulfide minerals such as pyrite oxidize and produce sulfuric acid; concurrently, iron and other metals are released into the water. The problem can be associated with both coal and hard rock operations where previously-buried sulfide minerals are exposed to oxygen and water. The descriptions of the bio-geochemical reactions responsible for ARD are found in many ASMR papers and will not be repeated here. However, it is prudent to revisit the general conditions required for ARD to form.

#### ARD Tetrahedron Relationship

Considered simply, the elementary ingredients required for the formation of ARD are analogous to the components needed for the burning of combustible materials. To have a fire, one must have air, heat and a fuel source. To have ARD, one needs air, water, and a pyrite

source and the bacteria to speed reactions that would otherwise occur slowly: consider an "ARD

Tetrahedron" concept (see Figure 1), with each requirement positioned at a vertex. If any of the primary ingredients are missing, isolated, or chemically neutralized, fire/ARD will not form. The oxidation of pyrite is an exothermic reaction very similar to conventional combustion. In some extreme cases pyritic mine wastes have actually spontaneously ignited (Li & Parr, 1926), resulting in localized sulfidic air pollution.



The tendency of a given rock or material to produce ARD is predicted by a number of standard tests, including acid-base accounting tests, humidity cell tests, and column leach tests.

## **Active Ingredients That Can Suppress ARD Production**

Researchers and practitioners of water pollution mi tigation have identified various active ingredients that can be applied to potential water pollution situations both within the mining industry (including ARD production) and in similar conditions (e.g., road construction). Many of these concepts have been successfully demonstrat ed on laboratory scale, but only a few have been tried at actual sites. The active ingredients include liquids, solid particles, gases, and livin g microbes; they are all designed to disrupt the ARD Tetrahedron relationship (Figure 1) and thereby prevent or suppress ARD. Examples of each active ingredient type follow.

## **Liquid Active Ingredients**

Olsen, et al. (2006) provides a comprehensive discussion of ARD-suppressing liquid reagents which is summarized and expanded here. Examples of liquid active ingredients include: sodium lauryl sulfate, a common surfactant identified as a bactericide that mitigates the oxidation of the mineral pyrite, bi-polar lipids (Zhang et al., 2003 ), and sodium thiocyanate appear to have a similar effect. Sodium hydroxide and hydrated lime solutions can adjust the pH of acidic pore water in contact with pyritic rocks and thus suppress ARD-generating bacterial activity.

Additional examples of liquid active ingredients in clude solutions of dissolved potassium permanganate (KMnO<sub>4</sub>) which has been shown to coat particulate mine was te materials with a layer of manganese dioxide and isolate pyritic rock from air and water and thus suppress ARD

formation. Waste milk has been shown to encourage a bio-film of bacteria that out-compete the suite of acid-generating bacteria and it also creat es a reducing environment inimical to oxidizing bacteria and provides nutrients for sulfate-reducin g bacteria (Jin et al., 2008 and ITRC, 2011). Solutions of dissolved phosphate have been shown to complex with dissolved iron and starve bio-oxidation of pyrite through disruption of the k inetics of ARD formation. However, use of this active ingredient has undesirable consequences if it is not properly controlled because it is a microbial nutrient. Silicate-based liquid active i ngredients that coat the surfaces of pollution-prone materials have also been developed (e.g., Keeco Mix (Mitchell et al., 1999)).

While not practical in typical situations, waste pa int might be used to suppress pyrite oxidation and prevent ARD.

## Solid Active Ingredients

Examples of solid active ingredients include: • limestone, dolomite, cement kiln dust, steel slag, sodium bicarbonate, fly ash and other coal combustion by-products, and various pozzolanic materials which can provide acidneutralizing alkalinity to pyritic rocks and mine wastes which are prone to produce ARD; • slow-release bactericides (Rastogi, et al., 1986) s uch as the commercial product ProMac<sup>TM</sup> which can suppress pyrite oxidizing bacteria; • organic materials such as cellulose, wood, paper, bio-solids, animal and vegetable protein whose decay can create conditions that suppress pyrite oxidation and ARD; and • processed peat, natural peat, zeolite minerals, man ganese oxides, and similar man-made products such as resins known to adsorb heavy metals. Additional examples of solid active ingredients inc lude: zero valent iron, nano-scale iron,

powdered iron oxy-hydroxides, and powdered copper.

chemically alter dissolved pollutants and as a result, detoxify them.

These materials have the ability to

#### Gaseous Active Ingredients

Examples of gaseous active ingredients include: ca rbon dioxide or nitrogen which can displace oxygen in the pore spaces in unsaturated, particulate mine wastes and thereby suppress ARD production; and hydrogen sulfide which also may have a similar effect as well as immobilizing heavy metals that may be in solutions in contact with particulate mine wastes. While using gaseous ARD suppressing materials is theoretically possible, their use to date has been minimal. Oxygen depletion through encapsulation or total, permanent immersion in weakly oxygenated water is a passive approach to ARD management.

## Microbial Active Ingredients

Examples of microbial active ingredients include co mmon materials that typically include bacterial suites including the bacteria *Desulfovibrio*, which under certain conditions and in the presence of other cellulose-degrading bacteria can out-compete *Acidithiobacillus ferro-oxidans* and thus suppress ARD (Zhang, et al. 2003). Common microbial source active ingredients may include municipal sewage bio-solids, composted anim al manure, and organic soils harvested from natural wetlands.

Table 1 below summarizes some common ARD-suppressin g materials available and what vertex of the ARD Tetrahedron they are known to suppress, but delivering these to large volumes of materials or areas has been problematic, especia lly if the materials are deposited or encountered in an unsaturated condition.

Table 1 – Summary of Materials Known to Suppress ARD

Basic ARD Ingredient	The "Geo-Medicines"	Anticipated ARD-Suppressing Reaction
Air	Fresh or composted wood chips, sawdust, or cellulose Mushroom compost Animal & vegetable protein Municipal sewage bio-solids Paper products	Consumes oxygen by organic decay
	Nitrogen Carbon dioxide	Displaces air/oxygen
Water	Potassium permanganate solutions Keeco Mix (micro-silicate) Bentonite clay Paint (latex or oil-based) or other water-resistant coating material	Coats reactive surfaces to render them impermeable

Basic ARD Ingredient	The "Geo-Medicines"	Anticipated ARD-Suppressing Reaction
Sulfides	Chitorem <sup>TM</sup>	Add organic matter and alkalinity
	Limestone	
	Dolomite	
	Kiln dust	
	Sodium bicarbonate	
	Alkaline Fly ash	Neutralize acidity/add alkalinity
	Flue gas desulfurization waste	
	Pozzolanic materials (cement)	
	Steel slag	
	Lime solution	
Sulfides	Sodium hydroxide solution	
(Cont).	Ammonia solution	
Bacteria	Sodium lauryl sulfate (aka shampoo)	
	(Kleinmann, 1982)	
	Alkyl-benzene sulfonate (aka laundry	
	detergent)	
	Milk	Bactericide
	Bi-polar lipids	
	Potassium Humate (Leonardite)	
	Sodium thiocyanate solution	
	Phosphate solution	
	Composted animal manure	Inoculate ARD-prone rock with beneficial bacteria (Jin et al., 2008)
	Municipal sewage bio-solids	
	Natural soils from wetlands	

## **Limitations of Conventional Active Ingredient Application**

Many of these pollution mitigation strategies and methods were patented but have not been widely applied despite their potential to solve a specific ARD problem. The primary reason for this aspect relates to the inability of practitioners to deliver and apply active ingredients to large volumes of potentially-ARD-generating materials. We hen active ingredients are carried in a conventional suspension or slurry (for solids) or a conventional solution (for liquids), there is much waste and little if any hydrologic control. To his is especially true when the liquids are injected into permeable materials such as a pile of mine waste rock or coarse coal refuse.

For example, the injected fluids are drawn by gravity toward the bottom of the pile with little horizontal dispersion; multiple injection boreholes — with close spacing may be required to effectively deliver the active ingredients to the waste horizon target. Excess fluids drain out the

bottom of the pile and may be difficult or impossib le to capture and recycle. However, the process has been demonstrated (see Fisher Coal Mine below).

## Case Studies of Conventional Active Ingredient Application

#### 1996 - Fisher Coal Mine, PA

A pumped injection technique for suppressing ARD is well-documented in Plocus and Rastogi (1997) which required four deep injection w ells [16 m (53 ft) deep] and 25 shallow injection wells 3 m (10 feet) deep to treat only ab out 1,200 m<sup>2</sup> (0.3 acres) of a coal mine waste pile in Pennsylvania. In order to implement their injection plan, pumping equipment with a pressure capacity of 20.7 megapascals (3,000 psi) was required. The active ingredients they used were a 20% solution of sodium hydroxide followed by a 2% solution of sodium lauryl sulfate, injected sequentially. While the process worked and the treatment appears to still be working 16 years later (Plocus, 2011), the technology was not considered practical.

#### 1996 - Fran Coal Mine, PA

Schueck et al. (1996) reported on treating pods of pyritic material in a backfilled surface coal mine pit with FBC ash grout in three ways:

- 1) injection grouting only,
- 2) capping only, and
- 3) both capping and grout injection.

Based on the water chemistry results from monitorin g wells, Option 3 worked the best followed by Option 1. Schueck et al. (1996) reported:

The inability to control final grout placement is a major drawback of the injection process... Because the grout is a viscous fluid, it w ill tend to flow into high permeability zones when pumped into spoil under pressure. If the permeability within the [pyritic rock] pod is low, the injected grout m ay flow away from the pod instead of filling the voids within the pod as intended or else the well will accept very little grout. When this happens, AMD abatement will be limited or will not occur at all.

## 2003 - Neves Corvo Copper-Tin Mine, Portugal

Verburg et al. (2003), reported the results of a 30 -week monitoring humidity test cells filled with pyritic mill tailing paste to evaluate various ARD-prevention strategies. They found that "the bactericide-amended samples demonstrate consistently higher values for paste pH and lower

values for SC [specific conductance] than the other samples, both in the short term and long term". The results further demonstrated that the application of the bactericide had a beneficial effect (i.e., preventing growth and bacterial acitivity) during all stages of acid generation at this site. The effects of the bactericide application period. Contrary to the findings of Plocus described above, the authors believed that "under operational or post-closure conditions, periodic or continuous application of a surfactant-type bactericide is generally required to maintain effectiveness". This belief may be related to the perceived difficulty in evenly applying a bactericide to tailings in an operational environment.

## 2006 - Sequatchie Valley Coal Mine, TN

An injection/treatment process similar to the one described by Plocus and Rastogi was implemented at the Sequatchie Valley coal mine in Tennessee. In this case, waste milk and a bacterial inoculum (biosolids) were injected into mean ine waste that had been reclaimed and revegetated by the Western Research Institute (Jin, et al., 2008 and ITRC, 2011) in order to establish a bio-film of bacteria on the pyritic was te that would out-compete acido-thiobacillus ferro-oxidans and thereby prevent ARD.

While details are lacking, the technology was implemented in a 4 ha (10 acre) area exhibiting a seepage of about 0.12 m <sup>3</sup>/min. (30 gpm). Ground water upstream of the test plot exhibits typical ARD characteristics, depressed pH (5.5 to 6 .0 s.u.); the seepage downstream of the test plot exhibits a pH of 6.8 to 8 about four years after the initial injection event (ITRC, 2011).

#### Foam: An Innovative Active Ingredient Delivery Method

Foam is a two-phase fluid consisting of a gas component surrounded by a thin fluid phase that is developed with a soluble surfactant or soap. Research efforts are underway to use this engineered material to deliver ARD-suppressing lique id-phase active ingredients (e.g., bactericides) which can be entrained in or are a part of the foam structure. In addition, solid phase ARD-suppressing ingredients such as limestone, lime, steel slag, biosolids, or cement kiln dust can be entrained and suspended in the foam structure. Such mixtures comprised of ARD-suppressing components are hereafter referred to as phoam TM to distinguish it from common foams used in other industrial applications, including fire-fighting.

The proposed pHoam TM method solves the active ingredient delivery problem by increasing the mobility and surface area of solutions or mixtual results of active ingredients without sacrificing

hydrologic control. Active ingredients suspended o r contained in a pHoam <sup>TM</sup> of pre-determined "stability", can flow omni-directionally or bi-dire ctionally from a single injection point as an advancing front. The density of the pHoam <sup>TM</sup> composites will typically be less than 320 kg/m <sup>3</sup>, which should lower injection pressures and increase the injection duration and coverage from each injection point.

# pHoam<sup>TM</sup> Stability

The term "stability" used here refers to the genera 1 characteristics of the mixture with regard to longevity of the foam structure, its density, wa ter content, and fluidity. For example, a pHoam<sup>TM</sup> could be designed to be thick enough to resist being drawn by gravity to the bottom of a given zone being treated and would advance in three edimensions, as a bulb. It could also completely fill an underground mine adit or coal mine entry. It would be expected to penetrate any roof falls as long as the collapsed material was permeable.

Alternatively, the pHoam TM mixture could be designed with a high "slump" (usi ng a term familiar to those dealing with concrete designs) that would fan out generally in two dimensions, following a horizontal plane as in the case of cove ring a relatively flat tailings surface or following the floor of an open pit or pit bench or mine adit/entry.

pHoam<sup>TM</sup> longevity can be manipulated to a desired time req uired for maximum treatment or travel through the material treated. For example, if a pHoam<sup>TM</sup> were to be applied to acidic mine waste on a truck load by truck load basis, the pHoa m<sup>TM</sup> structure might only need to persist for an hour or less, as long as the pHoamTM permeates t he entire load. Conversely, pHoam TM injected into a waste rock dump might be designed to persist for several days to allow maximum penetration.

The water content of pHoam <sup>TM</sup> can be adjusted to produce a relatively dry pHoam <sup>TM</sup> which barely changes the moisture content of the rock mas s being treated. When the bubble structure collapses, the entrained moisture will coat the nea rby rock particles. If the rock mass has a relatively high field capacity, a soil characterist ic, compared to the moisture content of the pHoam <sup>TM</sup>, little if any leakage from the treated mass should result. The active ingredients, both liquid and solid, should remain within the waste mass and not flow or rinse out.

Conversely, a high water content pHoam TM might be used to rinse out undesirable target contaminants from the mine waste. For example, a high water content pHoam TM could rinse out

retained nitrate contamination derived from blastin g agent residue in a waste rock dump that would otherwise require an extended period to be fl ushed out by pulses of infiltration of rain or snow melt.

## The Physics of pHoam<sup>TM</sup>

As discussed by Blauer and Kohlhass (1974):

Generally, foams are dispersions of a relatively la rge volume of gas in a relatively small volume of liquid. When the volume of liquid is considerably greater than that of gas, the gas bubbles are, as a rule, spherical and their mutual interaction is weak. These systems are known as "gas emulsions." In a true foam, the bubbles are so crowded that their shape is deformed, usually polyhedral.

Since the pHoam <sup>TM</sup> is mostly comprised of a gas phase with very littl e liquid (e.g. foam might be formulated to be 10% water and 90% gas), the liquid is more likely to be retained as a coating on the rock particles when the foam structure de-stabilizes. If a solid phase is present in the pHoam <sup>TM</sup>, it is more likely to be deposited on the surfaces of the mine waste instead of being carried away by gravity drainage in a conventional slurry suspension. Polymer additives can also be used in conjunction with pHoam <sup>TM</sup> composites. The polymer can bond the active ingred ients to the mine waste.

Also, as the solid phase is a relatively small volumetric component of the pHoam TM mass, it is difficult to completely fill the pore spaces between the permeable mine waste particles. This is a desirable condition, as it allows multiple events of active ingredient injection; i.e., a "booster shot" of antibiotics is required if the active ingredients are consumed and require replenishment.

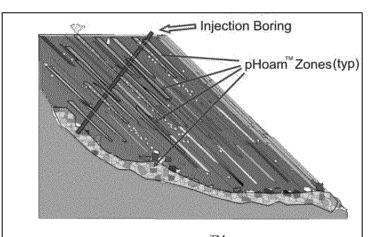


Figure 2. Injection of pHoam TM into a Mine Waste Dump (after G. W. Wilson, 2008)

The particle size distribution of the mine waste will certainly influence pHoam TM designs. Consider the heterotrophic nature of a typical mine waste dump (Figure 2). Due to the natural particle size segregation associated with end-dumping from trucks over the edge, a zone of larger

waste particles will be typically found at the toe of each lift. These high-permeability zones can act as preferred pathways for air and water which w ill promote ARD formation. Injected pHoam would also follow these preferred pathways, deposi ting ARD-suppressing reagents where they could provide the highest benefit. Fine -grained zones adjacent to coarser zones would tend to "wick" the liquid phase of active ing redients into the matrix and retain it with capillary force. The wicking could be facilitated by the decreases in surface tension provided by the surfactant component of the pHoam TM. It is likely that solid phase ARD-suppressing reagents would be deposited adjacent to the finer-g rained zones as a "rind" of beneficial treatment.

## The "Cyber-Knife" Effect

It is well known that pyrite oxidation is exothermi c. This reaction can result in elevated temperatures in mine waste and in the worst situati on, actual combustion. Common sense suggests that when foam or pHoam TM approaches materials with elevated temperatures, the foam/pHoam bubble structure will collapse as the liquid component evaporates. This feature could potentially give pHoam TM a "heat-seeking missile" capability that could automatically deliver more ARD-suppressing active ingredients to a mine waste site in the zones where it is needed the most. Hot zones in the mine waste would become "sinks" for pHoam TM bubble disintegration and resultant preferential deposition of more active ingredients compared to cooler zones nearby. Adopting the medical analogy, this is similar to a cyber-knife application to a specific diseased target organ without the need for an equivalent MRI image.

## Potential Application Situations – Medicine or Vaccine?

When does ARD-prone rock get infected? Conventiona 1 wisdom suggests that freshly-excavated rock containing pyrite has a relatively s mall acidophilic population when it is being excavated from a working face in a mine. Prolifi c infection with acidophilic bacteria does not appear to be instantaneous and sometimes months may pass before low-pH ARD is exhibited in runoff and/or seepage. The whole point of adding a lkalinity to satisfy acid-base accounting based ARD-suppression criteria is to allow the amen dments to collectively behave as a preventive "vaccine" to suppress acidophyllic bacterial activity. Wilson (2008), in his discussion of cover installations on waste rock, suggests that ARD prevention as the waste is placed should help to minimize future ARD treatment liability.

It is uncertain how long a bactericide needs to be contact with the target organism to be effective. However, from a pHoam TM perspective, a diluted pHoam recipe whose bubble structure decays in less than an hour (i.e., one with a relatively low "stability" as previously discussed) might be analogous to a "weakened virus" that would deal with human or animal disease. This is an topic that could benefit from future research.

Logic would therefore suggest that the amount of AR D-preventing "pHarmacueticals" may be less (and therefore less expensive to apply) as a preventive vaccine compared to the amounts needs to "medically" address a larger, more-establi shed and problematic acidophyllic microbial community. In other words, applying an ARD prevent ive vaccine may be much more cost effective than waiting until mine closure to addres s this issue. To be effective, however, vaccination efforts must be thorough as even small volumes of un-vaccinated ARD-prone rock could eventually re-infect adjacent treated areas. The re-infection mechanism is another topic that could benefit from future research; or: shoul d standard humidity cell tests be inoculated with acidophyllic bacteria?

## **Equipment**

The production of pHoam <sup>TM</sup> uses common construction equipment including tanks , mixers, compressors, reagent feeders and piping. Foam gene ration equipment typically has no moving parts. For example, a photo of an in-line static mixer is shown in Figure 3. A schematic layout of a pHoam <sup>TM</sup> system for treating a heap leach pad is provided i n Figure 4; while the equipment spread may appear simple, the innovation in the technology lies in designing the pHoam <sup>TM</sup> with the desired stability that matches the ARD-suppression situation.

Because up to 90% of the pHoam TM composite is a gas, large volumes of mine waste (o r mine voids) can be treated using minimal amounts of water and active ingredients.



Figure 3. Static mixer used to combine solid and foam components to create  $pHoam^{TM}$ 

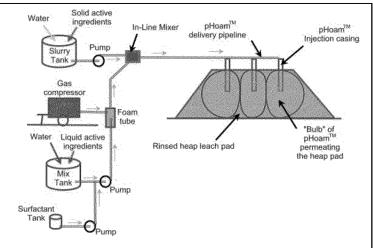


Figure 4. Example pHoam<sup>TM</sup> System Schematic Layout

## **Laboratory Test Work**

## Static Test Coating of Coarse Grained Rock

Practitioners in the petroleum industry have been injecting foams into porous media since the 1970's as evidenced in the technical literature (e. g., Blauer and Kohlhass (1974)) but the geological settings were significantly different from those faced by the mining industry. To validate the technology with regard to ARD-suppress ion, the authors conducted several laboratory scale demonstrations. The first demonstory action validated that a pHoam mixture could be developed to coat large particles of rock with a thin layer of fine-grained limestone with little water. Figures 5A through 5B compare the initial pHoam application on the left with the limestone-coated rocks about an hour later on the rock in Figure 5C is a close-up photo of the rock surface with a safety pin for scale; the rock in Figure 5D exhibits a coating (estimated <1mm thick) on the treated surface.

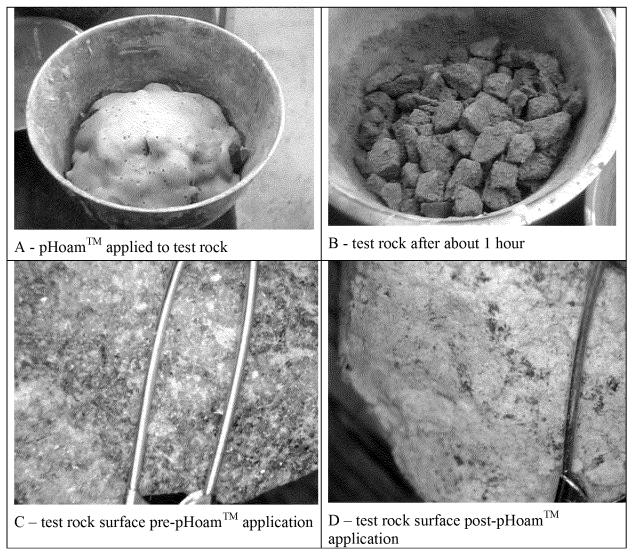


Figure 5. Laboratory application of pHoam<sup>TM</sup> to a clean gravel test rock

# pHoam<sup>TM</sup> Injection into Coarse-Grained Rock Filled Column

The authors next filled a 150 mm diameter 2.1 meter—long clear plastic tube with test gravel (nominal diameter 25mm particles) after inserting a—garden hose tremmie pipe into the sealed bottom of the pipe. The tube was positioned at a r—eclining angle of about 20 degrees on a sawhorse support. The pHoam TM injection rate was on the order of 0.75 liters per—second (12 gpm). The void space in the tube was estimated to—be about 15 liters (40% voids). The pHoam TM advanced in a steady front from the bottom to the—top of the tube in about 20 seconds after which the pHoam TM feed was suspended. However, the pHoam TM continued to expand and fill voids in the gravel after the feed was suspended. See Figure 6.



Figure 6. Gravel in column is encapsulated with pHoam<sup>TM</sup> after feed was suspended

A similar test was conducted with a 50 mm (2-inch) diameter column filled with 1.5 kg of relatively dry pea gravel (moisture <1%). The voids in the column were completely filled with a pHoam TM generated with 72 mL of liquid containing a sodium lauryl sulfate surfactant. The pHoam was designed to be stable for 12 to 18 hours. As a result of the application/injection, the moisture content was increased by about 4.8%. The final apparent moisture content of about 5.8% was less than the field capacity of the materi al, so the liquid content of the pHoam TM appeared to evenly coat the pea gravel after the bubble structure collapsed.

#### Costs

It can be safely projected that the more "stable" the pHoam<sup>TM</sup> mixture is, the more expensive it will be due to increasing surfactant requirement s. Preliminary cost estimating model results suggest that treatment costs will be primarily influenced by:

- 1. surfactant type there are natural, protein-based surfactants that may double as oxygendepleting active ingredients
- 2. surfactant strength a short-lived ARD pHoam TM "vaccine" formulation may not require as much surfactant as one designed to persist for several days and travel great distances (several hundred meters) in a "medicinal" formulation being injected into a thoroughly-infected mine waste mass (e.g., mine waste or coal refuse dump)

- 3. Cost of solid active ingredients (e.g., biosolids, alkalinity sources)
- 4. Cost of liquid active ingredients (e.g., water-solu ble organic materials or alkalinity sources or non-surfactant bactericides)

Labor and equipment costs per tonne or cubic meter of mine waste treated are expected to be less than 20 percent of the total on preliminary ec onomic estimates. The preliminary cost estimating model results were strongly influenced by the values assumed for the active ingredients.

For example, some municipalities currently pay ove r US\$316 per dry tonne to dispose of biosolids [20% solids by weight] produced from wast e water treatment plants (Carollo Engineers, 2008). If biosolids, which are predominantly comprised of organic carbon, are found to be a suitable solid-phase ARD suppressing material, and a municipality was willing to pay a ost, the "credit" from this income stream mining company a fraction of its current disposal c could significantly offset surfactant, labor and eq uipment costs and final cost of ARD prevention using the pHoam TM technology may be very low and sustainable. In an ideal situation, the mining company (or any other public, private, and non-profit entity) utilizing the pHoam<sup>TM</sup> process to deliver ARD-suppressing materials that others consider a waste might actually turn a small profit. Of course, as soon a s the municipality discovers that there is a market for their biosolids/waste material, the price may escalate. Procuring multiple sources of a given active ARD-suppressing ingredient well in advance would be advised.

If biosolids' application as an ARD-suppressing mat erial is practical, why has it not already been used? The answer, as with any other material in the "ARD pHarmacy", is likely that a practical way of delivering it to coat large volume sof mine waste has not been available. Perhaps this situation is no longer true.

#### **Summary**

The pHoam TM ARD-suppression technique is an emerging technolog y and the potential advantages of treating large volumes of mine waste with little water have yet to be fully developed. The technology could find application a t both active and abandoned mines, either underground or surface, and could address mine wast es such as tailings, waste rock and even backfill in pits that have been fully revegetated w ithout re-disturbance. The design of pHoam TM applications will be site specific, and will depend on the grain size, geochemistry, and in-place

permeability of the mine waste, among other factors  $\,$ . It does not appear to be appropriate for application in fully-saturated or flooded condition  $\,$ s although pHoam  $^{TM}$  with a density heavier than water is possible.

## Future Study and Technology Development

Much study remains to advance the pHoam <sup>TM</sup> ARD-suppression technique from an emerging technology to a best management practice. As such, the authors are seeking demonstration sites that ideally exhibit the following conditions:

- Has research funding available
- Contains mine waste that is fully characterized, mapped, and is acid generating
- Is an active mine site/plant with a steady, consist ent stream of acid-prone waste (e.g., coarse coal refuse or coarse tailings) that could be evaluated in test piles or lined test containers
- Is relatively small in scale (0.5 to 1 hectare) (1 to 2 acres)
- Is relatively accessible by conventional construction equipment
- Is amenable to "dissection" after pHoam TM application
- Has documented ARD impact
- Is on publicly-owned land (USFS, USBLM, USEPA Superfund)
- Is not a part of or contingent upon ongoing litigation

To quote a Latin proverb: *Nihil simul inventum est et perfectum*. [Nothing is invented and perfected at the same time.]

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